



# Avalanches in fatigue and crossover from creep to fatigue

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31.8.2022

# What is fatigue?

- ▶ Material response to repetitive loading
- ▶ Important for many practical applications



SS Schenectady

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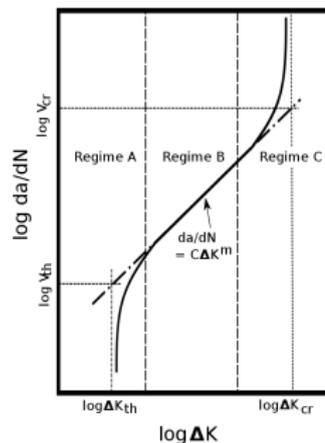


SS Schenectady

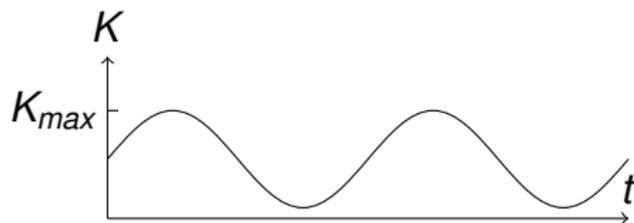
- ▶ Apparent self-similarity (Paris–Erdogan law)

$$\frac{da}{dN} \propto \Delta K^m$$

- ▶  $a$  crack length
- ▶  $N$  loading cycles
- ▶  $K$  stress intensity factor
- ▶  $\Delta K = K_{max} - K_{min}$



# Fatigue protocol

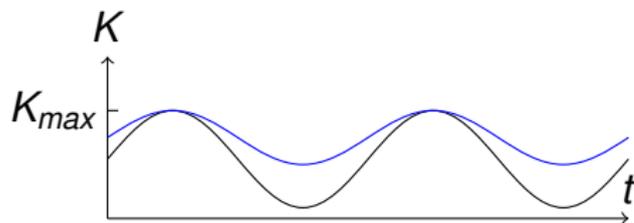


$$R = 0.1$$

► Asymmetry coefficient

$$R = \frac{K_{min}}{K_{max}}$$

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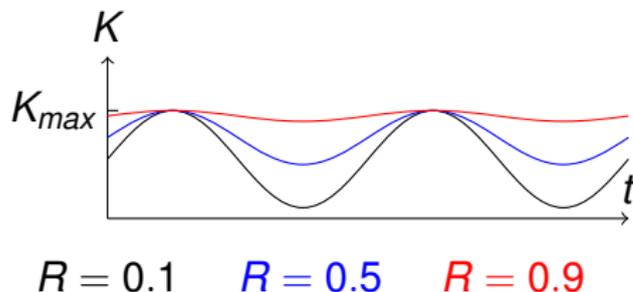


$$R = 0.1 \quad R = 0.5$$

- ▶ Asymmetry coefficient

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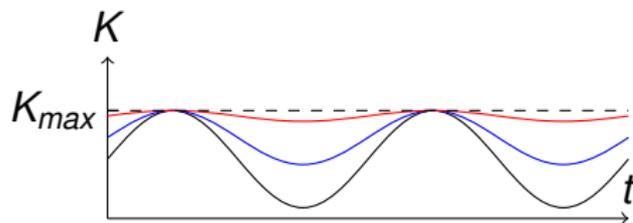
# Fatigue protocol



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# Fatigue protocol



$R = 0.1$      $R = 0.5$      $R = 0.9$

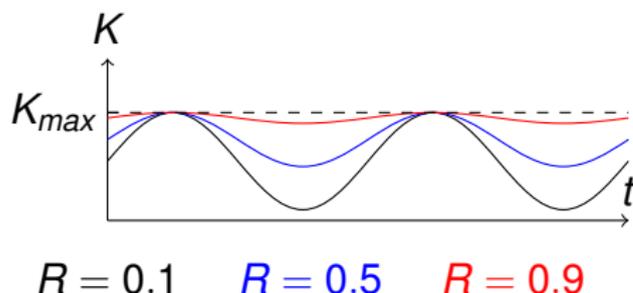
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$$R = 1$$

# Fatigue protocol



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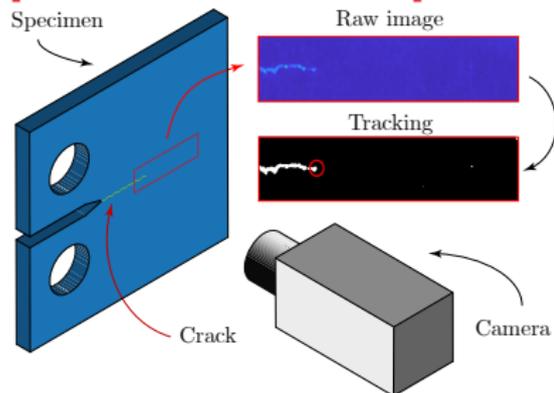
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- ▶ the goal here is to explore the intermittent crack growth in fatigue [Kokkonen et al, JSTAT 2017] and the crossover to creep
- ▶ sort of similar to the Oslo Plexiglas experiments [Måløy et al, PRL 2006] but for a geometry more commonly used in the field of material science

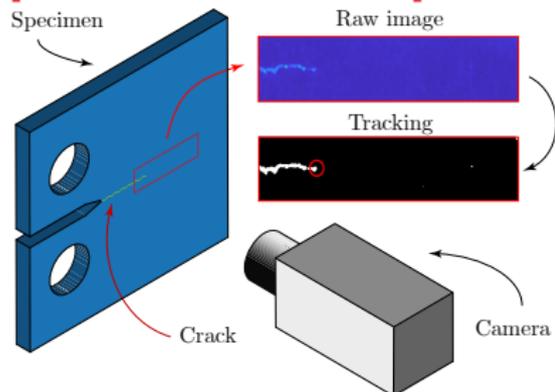
# Experimental setup



Lomakin et al, PRRResearch 2021

- ▶ CT-specimens of 1050 Al alloy
- ▶ 10 Hz loading frequency, 0.25 Hz imaging frequency
- ▶ crack tip position tracked from the images

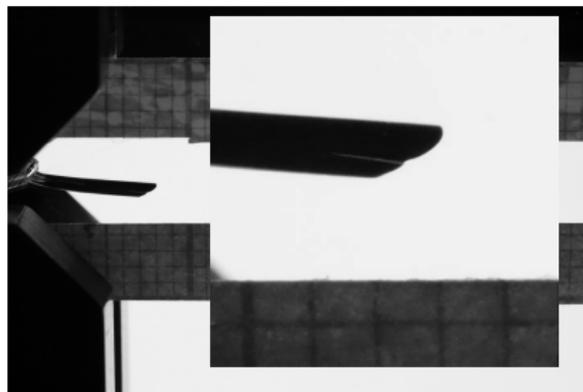
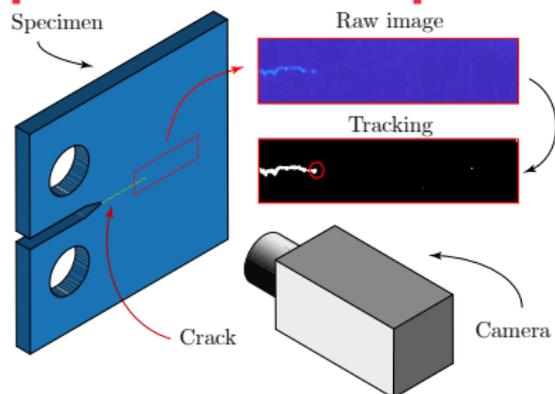
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- ▶ transparent PMMA
- ▶ placing the camera at an angle allows the tracking of a fracture line
- ▶ 1 Hz loading frequency, 1 Hz imaging frequency

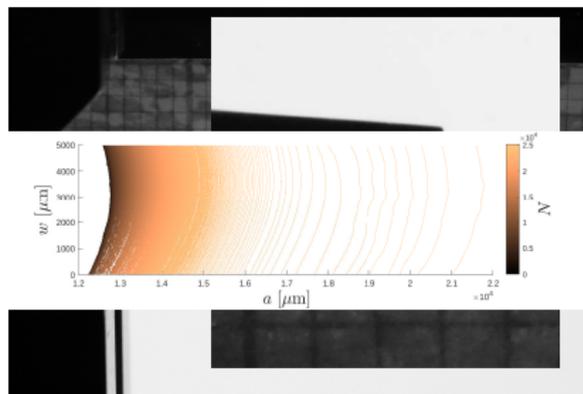
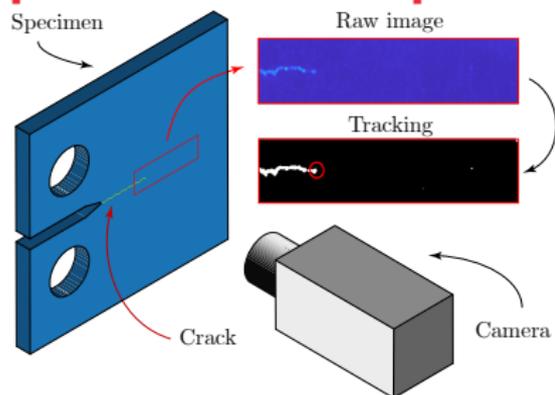
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# Naive attempt from creep to fatigue

Thermally activated process  $v = v_c \exp(-\beta \Delta E)$

Below depinning threshold  $\Delta E = \frac{1}{\beta_d} \left[ \left( \frac{G}{G_c} \right)^{-\mu} - 1 \right]$ ,  $G \propto K^2$

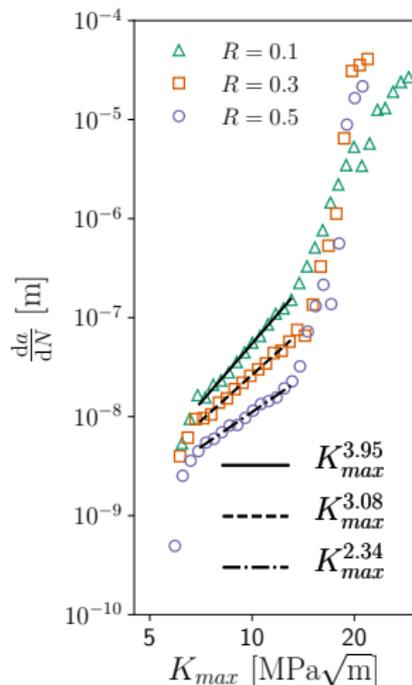
Integrate the velocity over the loading cycle

$$v_{fat} = \frac{\Delta a}{\Delta N} = \int_0^{1/f} v dt = v_c e^{\frac{\beta}{\beta_d}} \int_0^{1/f} \exp \left[ -\frac{\beta}{\beta_d} \left( \frac{K(t)}{K_c} \right)^{-2\mu} \right] dt$$

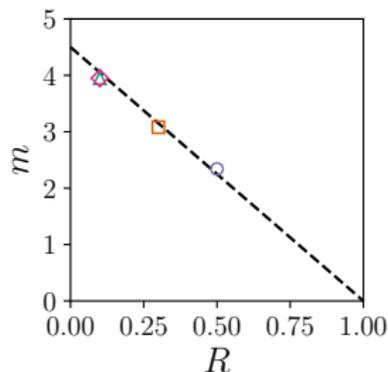
where  $K(t) = \frac{K_{max} + K_{min}}{2} + \frac{\Delta K}{2} \sin(2\pi ft)$

Saddle-point integration gives  $v_{fat} \propto K_{max}^\mu \exp \left[ -\frac{\beta}{\beta_d} \left( \frac{K_{max}}{K_c} \right)^{-2\mu} \right]$

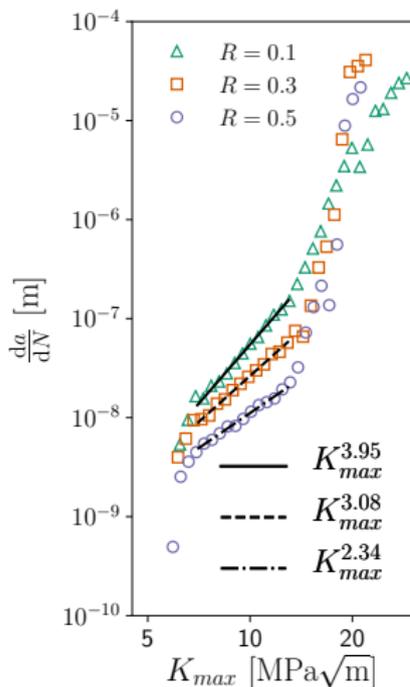
# Aluminum samples



- ▶ flattening of the Paris regime in the Paris plots
  - ▶  $m$  linearly decreases with  $R$

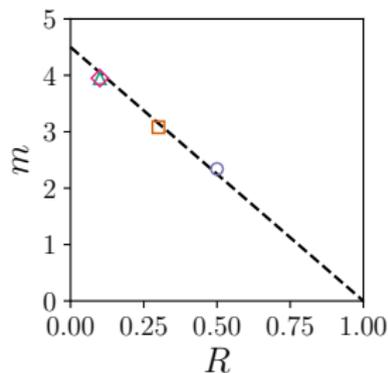
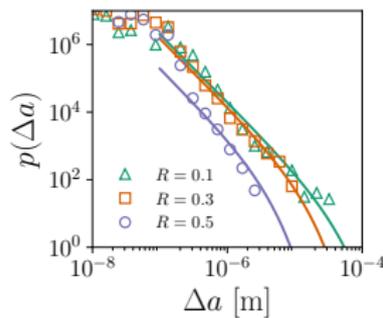


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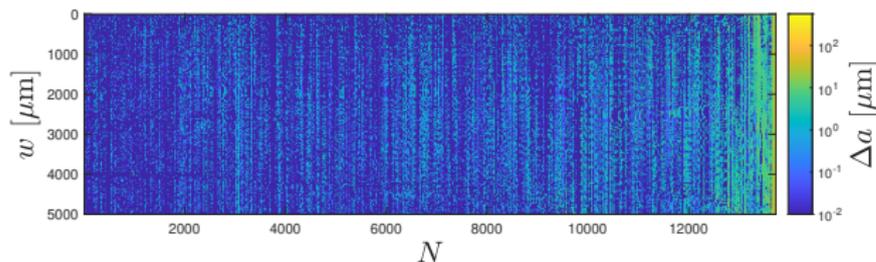
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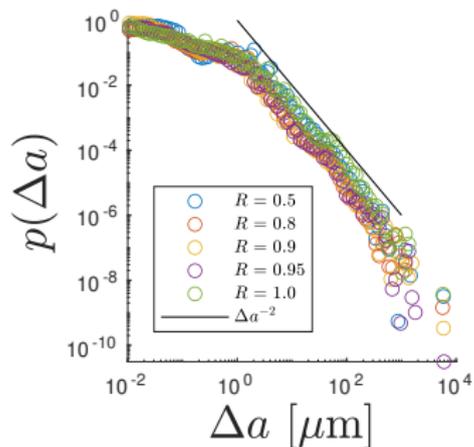
▶ power-law distributed jump sizes

$$p(\Delta a) \propto \Delta a^{-2} e^{-\frac{\Delta a}{\Delta a_0}}$$

# PMMA samples – local velocities

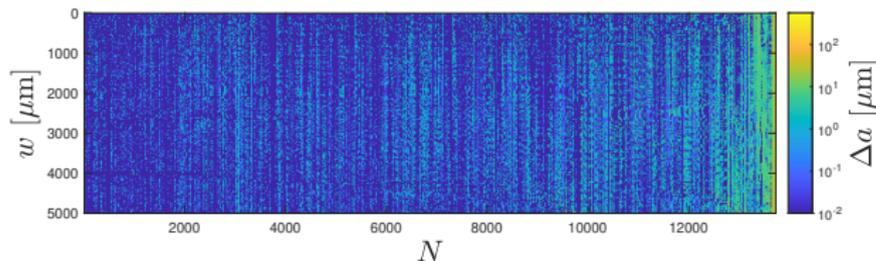


▶ velocity of a 1D crack line

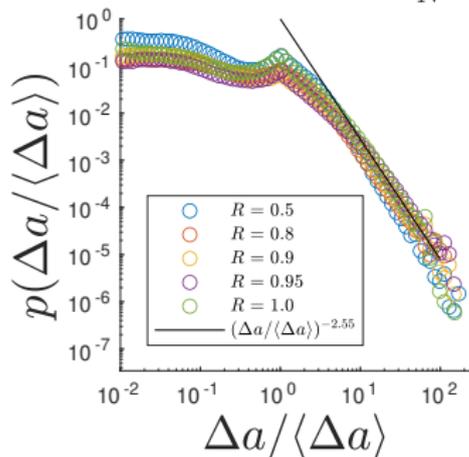


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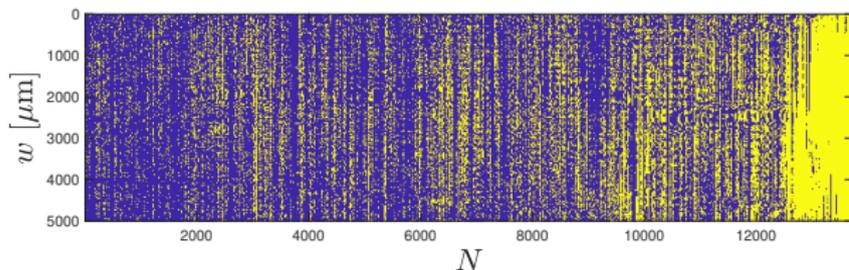


▶ velocity of a 1D crack line

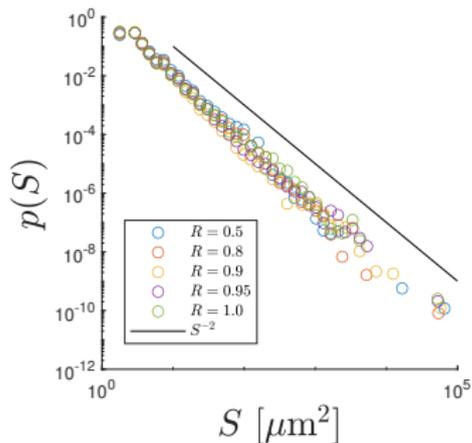


- ▶ a power-law distributed tail with an exponent of roughly 2
- ▶ not much variation in the distribution
- ▶ Oslo experiments [Måløy et al, PRL 2006] had an exponent 2.55 (for the normalized velocity)

# PMMA samples – avalanche sizes

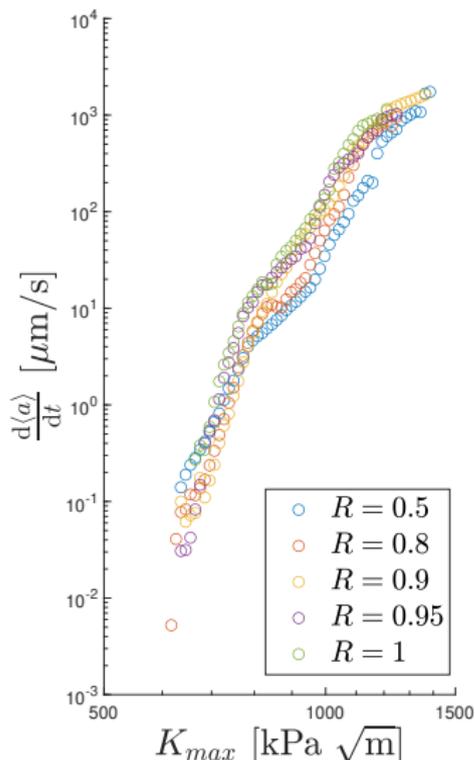


- ▶ the local velocity is thresholded to yield avalanche clusters



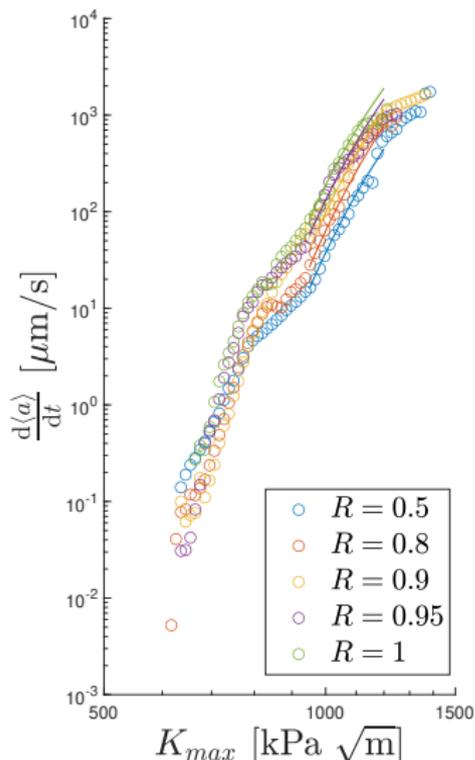
- ▶ still a power-law with an exponent of roughly 2
- ▶ again not much variation in the distribution
- ▶ Oslo experiments [Måløy et al, PRL 2006] had an exponent around 1.5-1.7 (some variation depending on the methodology)

# PMMA samples – Paris curves



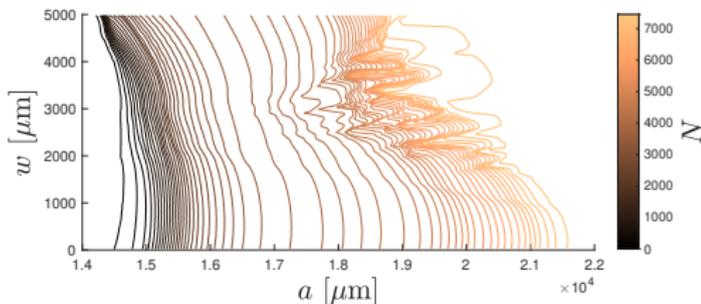
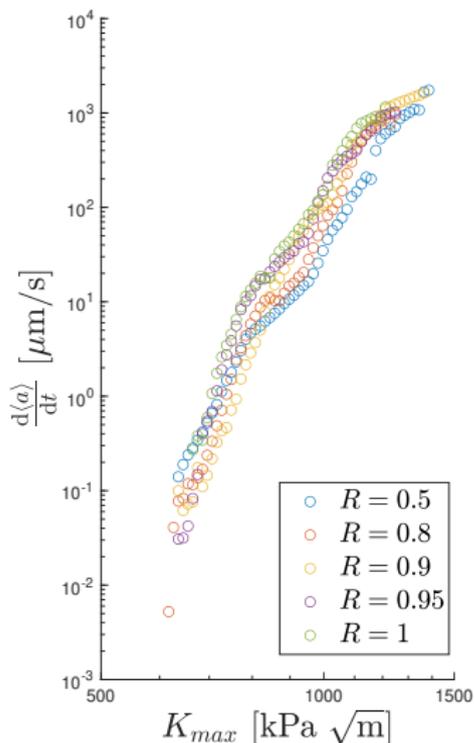
- ▶ the crack velocity considered as the time derivative of the mean crack position  $\langle a \rangle$
- ▶ there is a lot of sample-to-sample variation in this mean velocity
  - ▶ the variation seems to increase with increasing  $R$
- ▶ two regimes
  - ▶ related to the strain rate sensitivity of PMMA?

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- ▶ two regimes
  - ▶ related to the strain rate sensitivity of PMMA?
  - ▶ the naive brittle approach works for the end part of the experiments

# PMMA samples – front shape



- ▶ the large velocity fluctuations might be related to variations in the front shape
  - ▶ pinning at some defect

# Conclusions

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- ▶ our plan is to repeat same studies with glass
  
- ▶ somehow taking the front shape into account might also be good
  
- ▶ the local dynamics seem fairly constant with varying loading conditions
  
- ▶ the "universal" exponent of 2 is high
  - ▶ this might partially be explained by the nonstationarity of the velocity