# Investigation of avalanche phenomena by simultaneous measurements of different variables

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Avalanche Debrecen, August 30 2022

supported by Israel Science Foundation



# **Twin boundary motion**

- A crystal/grain can be separated into domains/twins that have different orientation of the unit cell.
- The interfaces between domain/twins are called twin boundaries.
- Mechanical stress / electric field / magnetic field ⇒ Expansion of the favored domain/twin-variant on the expense of other domains/twin-variants.

#### Examples:

- Domain switching in ferroelectric materials
- Twinning reorientation in ferromagnetic shape memory alloy (FSMA) NiMnGa



# **Example: Domain switching in ferroelectric BaTiO<sub>3</sub>**

Time: *t* 



Time: *t* + 0.6 μs

Twin Motion Faster than the Speed of Sound Faran and Shilo, PRL, (2010).

# **Example: Phase transformation in SMA**



Self similar propagation of the phase boundary and twinning microstructure

**Temperature** 

Analysis of austenite-martensite phase boundary and twinned microstructure in SMA Bronstein, Faran, and Shilo, Acta Mater, (2019).

## **Example: Plastic deformation in magnesium**

100,000 Frames Per Second

4 mm

High-rate nucleation and motion of twin boundaries in Mg single crystals *Faran and Shilo, to be published.* 

# **Example: Twinning reorientation in FSMA Ni-Mn-Ga**



Variability of twin boundary velocities in 10M Ni-Mn-Ga measured under µs-scale force pulses *Mizrahi, Shilo, and Faran, SMS, (2020).*  Many studies reported power law distributions of avalanches during the motion of twin boundaries in different materials

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3.2 ε~1.5 10<sup>1</sup> -30  $ln(v^2)$ 15mN/min 25mN/min 10 30mN/min s = 1.6 **E A** 10<sup>-2</sup> PbZrO, 10<sup>-4</sup> 10-11 10-13 10-12 10-10  $10^{-9}$ 10<sup>-6</sup>  $v_{2}^{2}$  (mm<sup>2</sup>/s<sup>s</sup>) S. Puchberger et al., APL Materials 5 (2017) 046102.



L. Daróczi, E. Piros, L.Z. Tóth, D.L. Beke, *Phys. Rev. B* **96** (2017) 014416.

V. Soprunyuk, S. Puchberger, A. Tröster, E. Vives, E. K. H. Salje, W. Schranz, J. Phys. Condens. Matter. **29** (2017) 224002. The characteristics and kinetic laws for twin boundary motion can be accurately modeled and predicted



# **Example: The twinning stress in various materials**



Twin Boundary Structure and Mobility Shilo, Faran, Karki, Müllner, Acta Mater, (2021).

# **Example: Twin boundary velocity vs. electric field in ferroelectrics**



Kinetics of domain wall motion in ferroelectric switching Hayashi, J. Phys. Soc. Japan, (1973).

# **Example: Kinetic relations for twin boundary motion in FSMA**





The kinetic relation for twin wall motion in NiMnGa Part I: Faran and Shilo, J. Mech. Phys. Solids (2011) Part II: Faran and Shilo, J. Mech. Phys. Solids (2013)

# **Example: Discrete twin boundary dynamic simulations**



Inertia controlled twinning in Ni-Mn-Ga actuators: a discrete twin boundary dynamics study *Faran, Riccardi, Shilo, SMS, (2017).* 

# The enigma of twin boundary motion

# Power law distributions of avalanche events

- The average and STD of a power law distribution are undefined or do not represent a typical (most probable) value.
- Avalanches are not governed by characteristic properties or kinetic laws.



Well predicted twinning stress and kinetic laws

 Some variables that characterize the twin boundary motion display a characteristic value or follow a kinetic law.

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# **Calls for measuring different variables during avalanche events**

Apply: controlled external/average strain

Measure: stress ( $\sigma$ ) vs. time (t)

$$\mathcal{E} = \frac{\Delta L}{L_0} = \frac{ct}{L_0}$$

c – applied displacement rate  $L_0$  - Sample's length

Applied strain: 
$$\mathcal{E} = \frac{ct}{L_0} = \frac{\sigma}{Y} + \mathcal{E}_{trans}$$

c – displacement rateY – effective modulus (stiffness)

Applied strain:



Strain due to twin boundary motion:

$$\mathcal{E}_{trans} = \frac{\mathcal{X}_{TB}}{L_0} \mathcal{E}_T$$

 $X_{TB}$  – twin boundary displacement  $\mathcal{E}_T = 0.06 - \text{twinning strain}$ 

 $\mathcal{E}_{trans} = \frac{X_{TB}}{L_0} \mathcal{E}_T$ 

Applied strain:  $\mathcal{E} = \frac{c_i}{L_0}$ 

$$\mathcal{E} = \frac{ct}{L_0} = \frac{\sigma}{Y} + \mathcal{E}_{trans}$$
  $c - displacement rate $Y - effective modulus (stiffness)$$ 

 $x_{TB}$  – twin boundary displacement  $\mathcal{E}_T$  = 0.06 – twinning strain

Variable 1: Twill boundary displacement during an avalanche event:

Strain due to twin boundary motion:

$$x_{TB} = \frac{c\Delta t}{\varepsilon_T} - \frac{L_0}{\varepsilon_T Y} \Delta \sigma$$

Released potential (elastic) energy during an avalanche event:

$$\Delta U_P \cong -A\sigma\varepsilon_T \cdot \Delta x_{TB}$$

Applied strain: $\mathcal{E} = \frac{CT}{L_0} = \frac{O}{Y} + \mathcal{E}_T$ oundary motion: $\mathcal{E}_{trans} = \frac{X_{TB}}{L_0} \mathcal{E}_T$ 

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<u>Variable 2:</u> Temporary twin boundary velocity:

Potential energy release rate:

$$\psi_{TB} = \frac{c}{\varepsilon_T} - \frac{L_0}{\varepsilon_T Y} \dot{\sigma}$$

$$\dot{U}_P \cong -A\sigma\varepsilon_T \cdot v_{TE}$$

Applied strain:  $\mathcal{E} = \frac{ct}{L_0} = \frac{\sigma}{Y} + \mathcal{E}_{trans}$ 

$$\varepsilon_{trans} = \frac{x_{TB}}{L_0} \varepsilon_T$$

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<u>Variable 2:</u> Temporary twin boundary velocity:

Potential energy release rate:

$$v_{TB} = \frac{c}{\varepsilon_T} - \frac{L_0}{\varepsilon_T Y} \dot{\sigma}$$

 $E_{AE}$ 

$$\dot{U}_P \cong -A\sigma\varepsilon_T \cdot v_{TB}$$

Variable 3: Total acoustic emission energy during an event:

### Two types of twin boundaries in Ni-Mn-Ga

ne

**200 µm** 

twin wal



$$\dot{\sigma} = \frac{Y}{L_0} (c - \varepsilon_T v_{TB})$$













- There are no time intervals during which the twin boundary motion stops.
- The twin boundary moves during all time but with different velocities.

# Statistical distributions of AE and twin boundary velocity during mechanical tests

#### Velocity - Gaussian distribution



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AE - Power law distribution

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10<sup>5</sup>

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#### A similar enigma for 90° domain wall motion in ferroelectric BaTiO<sub>3</sub>



• Well determined kinetic law

Power law distribution

#### Coexistence of a well-determined kinetic law and a scaleinvariant power law during the same physical process



#### Coexistence of a well-determined kinetic law and a scaleinvariant power law during the same physical process



# **Conclusions for type II twin boundaries**

The two different statistical behaviors reflect the mixing of different types of fluctuations:

**During most of the twin boundary motion:** 

Slow and mild non-critical fluctuations about an average value, predicted by a kinetic law.

**During short times:** 

Fast and abrupt avalanches that display a power law distribution.





- Time intervals during which the stress increases linearly, indicating that the twin boundary doesn't move.
- Distinct abrupt stress drops that occur during twin boundary motion.



Mechanical energy released during an avalanche:

$$\Delta U_m = \frac{F_{up}^2 - F_{down}^2}{2k}$$



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- 98.5% of the AE signals with an energy larger than 10 *aJ* were not associated with any detectable stress drop event.
- All values of  $E_{AE}$  are smaller by at least 7 orders of magnitude than the corresponding value of  $\Delta U_m$ .
- The overall AE energy is smaller by 8 orders of magnitude than the overall released mechanical energy.

#### Relations between stress drops and AE on the level of individual events



- 94% of the stress drop events were accompanied by an AE signal with an energy larger than 10 *aJ*.
- The probability of finding an AE event during a stress drop is ~ 100 times higher than between stress drops.

#### Stress drops vs AE signals on the level of individual events



• *E<sub>LB</sub>* is associated with macroscopic stress changes.

#### Analysis of AE events occurring during stress drops



The distribution of  $E_{AE}$  is centered about a peak that represents a typical value.

The distribution of  $\Delta E$  has a power law segment

The process that contributes to  $\Delta E$  is close to dynamic criticality.

Avalanche is manifested by a burst of twin boundary velocity











• The stress drop generates a wide band of acoustic waves, most of them with frequencies that scale as 1/∆t (sub kHz range) and are much lower than the frequency range captured by the AE transducer (above 100 kHz).

Therefore:  $\Delta U_m \gg E_{AE}$ 

### Shape of the $v_{TB}$ vs. *t* avalanche



# Shape of the $v_{TB}$ vs. *t* avalanche



# Shape of the $v_{TB}$ vs. *t* avalanche











# **Conclusions for type I twin boundary**

- There is no direct correlation between parameters measured by the force sensor  $(\Delta x_{TB}, \Delta \sigma, \text{and } \Delta U_m)$  and the AE sensor <u>during the same events</u>.
- There is a lower bound for  $E_{AE}$ , which is approximately proportional to  $\Delta U_m$ .
- The additional AE energy, above the lower bound, display a power law distribution, indicating that this contribution comes from local events that occur at much smaller scales (nm length scale and µs time scale).







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- Unified theories that explain both avalanche statistics and kinetic laws are highly desired.
- A first step toward obtaining such theories is to take simultaneous measurements of different variables.